

MICRO-OPTICS

Axetris AG

### INFRARED SOURCES Schwarzenbergstrasse 10

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#### MASS FLOW DEVICES

LASER GAS DETECTION

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# EMIRS200\_AT01T\_BR100

# Thermal MEMS based infrared source

For direct electrical fast modulation

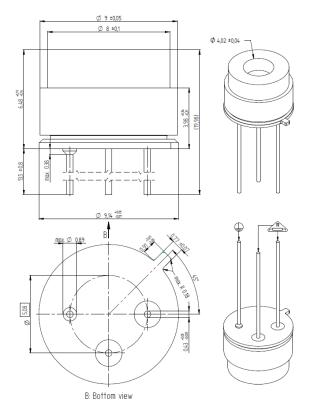
TO39 header with Reflector 2

#### Infrared Source

Axetris infrared (IR) sources are micro-machined, electrically modulated thermal infrared emitters featuring true blackbody radiation characteristics, low power consumption, high emissivity and a long lifetime. The appropriate design is based on a resistive heating element deposited onto a thin dielectric membrane which is suspended on a micro-machined silicon structure.

#### Infrared Gas Detection Applications

- Measurement principles: non-dispersive infrared spectroscopy (NDIR), photoacoustic infrared spectroscopy (PAS) or attenuated-total-reflectance FTIR spectroscopy (ATR)
- Target gases: CO, CO<sub>2</sub>, VOC, NO<sub>X</sub>, NH<sub>3</sub>, SO<sub>X</sub>, SF<sub>6</sub> hydrocarbons, humidity, anesthetic agents, refrigerants, breath alcohols
- Medical: Capnography, anesthesia gas monitoring, respiration monitoring, pulmonary diagnostics, blood gas analysis
- Industrial Applications: Combustible and toxic gas detection, refrigerant monitoring, flame detection, fruit ripening monitoring, SF<sub>6</sub> monitoring, semiconductor fabrication
- Automotive: CO<sub>2</sub> automotive refrigerant monitoring, alcohol detection & interlock, cabin air quality
- Environmental: Heating, ventilating and air conditioning (HVAC), indoor air quality and VOC monitoring, air quality monitoring



#### Features

- Large modulation depth at high frequencies
- Broad band emission
- Low power consumption
- Long lifetime
- True black body radiation (2 to 14 μm)
- Very fast electrical modulation (no chopper wheel needed)
- Suitable for portable and very small applications
- Rugged MEMS design



#### ■ Absolute Maximum Ratings (T<sub>A</sub> = 22°C)

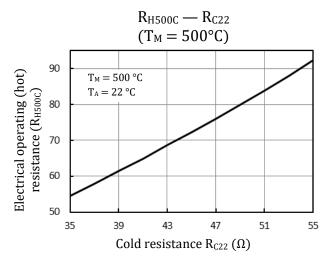
Parameter	Symbol	Rating	Unit
Heater membrane temperature <sup>1</sup>	Тм	500	°C
Optical output power (hemispherical spectral) $(T_M = 500^{\circ}C)$	P <sub>00</sub>	30	mW
Optical output power between 4 $\mu$ m and 5 $\mu$ m (T <sub>M</sub> = 500°C)	P <sub>s4-5</sub>	4.0	mW
Optical output power between 6 $\mu$ m and 8 $\mu$ m (T <sub>M</sub> = 500°C)	P <sub>s6-8</sub>	5.4	mW
Optical output power between 8 $\mu$ m and 10 $\mu$ m (T <sub>M</sub> = 500°C)	P <sub>s8-10</sub>	3.3	mW
Optical output power between 10 $\mu$ m and 13 $\mu$ m (T <sub>M</sub> = 500°C)	P <sub>s10-13</sub>	2.8	mW
Electrical cold resistance (at $T_M = T_A = 22^{\circ}C$ )	R <sub>C22</sub>	35 to 55	Ω
Electrical operating (hot) resistance <sup>2</sup> (at $T_M = 500$ °C with $f = \ge 5$ Hz and $t_{on} \ge 8$ ms)	R <sub>H500C</sub>	1.883 * RC22 – 12.02	Ω
Package temperature	T <sub>P</sub>	80	°C
Storage temperature	Ts	-20 to +85	°C
Ambient temperature <sup>3</sup> (operation)	T <sub>A</sub>	-40 to +125	°C
Heater area	A <sub>H</sub>	2.1 x 1.8	mm <sup>2</sup>
Frequency <sup>4</sup>	f	5 to 50	Hz

Note: Emission power in this table is defined by hemispherical radiation. Stress beyond those listed under "absolute maximum ratings" may cause permanent damage to the device.

Note: Diagram  $R_{H500C} - R_{C22} | (T_M = 500^{\circ}C)$ 

How to ensure that the maximum temperature for  $T_{\mbox{\scriptsize M}}$  is not exceeded:

- 1. Determine electrical cold resistance  $R_{C}$  of the EMIRS device at TA=22°C  $\,$
- 2. Ensure that anytime  $R_H$  does not exceed the representative limit as shown in this diagram with respect to these conditions:
  - a.  $f \ge 5 Hz$
  - b. on-time (pulse duration)  $\ge 8 \text{ ms}$



Electrical operating (hot) resistance  $R_H$  versus electrical cold resistance  $R_{C22}$  at  $T_A = 22^{\circ}C$ 

<sup>&</sup>lt;sup>1</sup> Temperatures above 500°C will impact drift and lifetime of the devices.

<sup>&</sup>lt;sup>2</sup> See Diagram  $R_H - R_C | (T_M = 500^{\circ}C)$ 

<sup>&</sup>lt;sup>3</sup> The environmental and package temperature might impact the lifetime and characteristic of the devices.

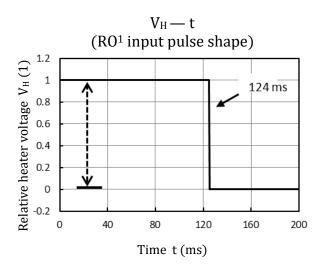
<sup>&</sup>lt;sup>4</sup> Lower cut-off frequency of 5 Hz for designed thermodynamic state.



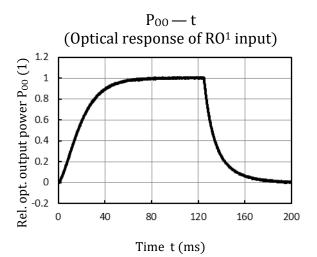
## ■ Ratings at Reference Operation (RO<sup>1</sup> T<sub>A</sub> = 22°C)

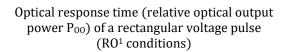
Parameter	Symbol	Rating	Unit
Heater membrane temperature	Тм	< 500	°C
Duty cycle of rectangular $V_{\rm H}$ pulse	D	62	%
Frequency of rect. pulse shape <sup>2</sup>	$\mathbf{f}_{ref}$	5	Hz
On time constant of integral emissive power $P_{00}$	$ au_{on}$	18	ms
Off time constant of integral emissive power $P_{00}$	$ au_{off}$	8	ms
Package temperature at $T_A = 22^{\circ}C$	T <sub>P</sub>	40 to 85	°C

Note: First order on-time model using  $\tau_{on}$ : First order off-time model using  $\tau_{off}$ :



 $\label{eq:Relative rectangular heater voltage (V_{H}) \ pulse \ with \ a \\ relative \ pulse \ width \ of \ 124 \ ms \ at \ 5 \ Hz \\ (time \ description \ of \ reference \ operation \ RO^{1})$ 



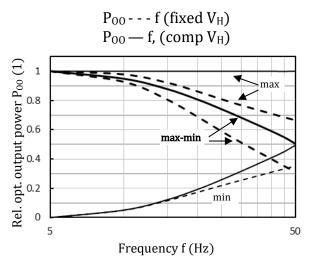


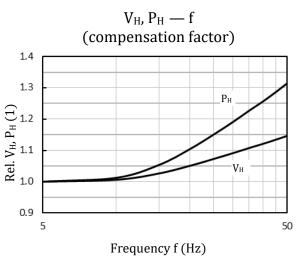
<sup>&</sup>lt;sup>1</sup> Reference Operation: combines lower cut-off frequency of 5 Hz and maximum modulation depth (max-min signal)

<sup>&</sup>lt;sup>2</sup> Recommended frequencies from 5 Hz to 50 Hz



#### ■ Typical Timing Characteristics Frequency (D = 62%)





Relative (to RO) max, min, max-min values of optical output power ( $P_{00}$ ) versus frequency f with fixed and compensated  $V_H$ 

Note: Diagrams a, b <u>Relative</u>  $P_{00}$ ,  $V_H$ ,  $P_H$  to reference operation (RO) f=5 Hz, rect. pulse D=62%

<u>max:</u> maximum value of  $P_{00}$  response shape <u>min:</u> minimum value of  $P_{00}$  response shape <u>max-min:</u> amplitude calculation of  $P_{00}$  resp. shape

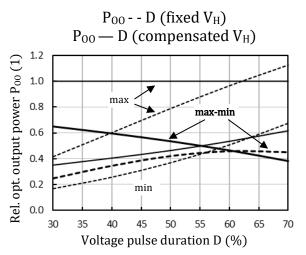
Fixed V<sub>H</sub>: same voltage for all frequencies.

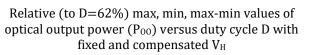
<u>Compensated</u>  $V_{H}$ : for every frequency value, the voltage is adjusted to achieve the same maximum of  $P_{00}$  response shape as for 5 Hz.

Relative (to RO) electrical drive values heater voltage  $V_H$  and power  $P_H$  versus frequency f for compensation



■ Typical Timing Characteristics Pulse Duration D<sup>1</sup> (f = 50 Hz)



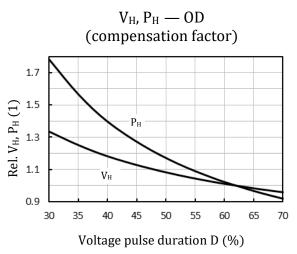


Note: Diagrams a, b <u>Relative</u>  $P_{00}$ ,  $V_H$ ,  $P_H$  to reference operation (RO) f=50 Hz, rect. voltage pulse

<u>max:</u> maximum value of  $P_{00}$  response shape <u>min:</u> minimum value of  $P_{00}$  response shape <u>max-min:</u> amplitude calculation of  $P_{00}$  resp. shape

Fixed V<sub>H</sub>: same voltage for all frequencies.

<u>Compensated</u>  $V_{H}$ : for every frequency value, the voltage is adjusted to achieve the same maximum of  $P_{00}$  response shape as for D=62%.



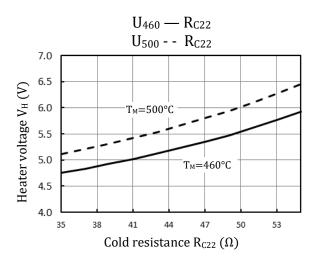
Relative (to RO) electrical drive values heater voltage  $V_H$  and power  $P_H$  versus duty cycle D for compensation

<sup>&</sup>lt;sup>1</sup> Effective D shorter than 30% and voltage or power compensation at high frequencies (e.g. 20% @ 50 Hz) might impact the lifetime and characteristic of the devices because of additional stress in material layers.



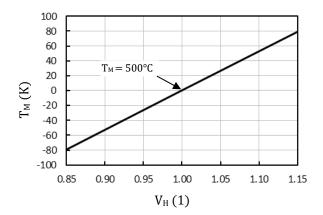
### ■ Typical electrical/thermal characteristics (RO, T<sub>A</sub> = 22°C)

Parameter	Symbol	Rating	Unit
Peak chip membrane temperature	Тм	460/500	°C
Heater voltage	$V_{\rm H}$	5.23/5.66	V
Heater power	P <sub>H</sub>	394/446	mW

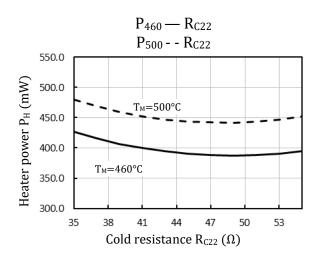


 $\label{eq:Mean1} Mean^1 \mbox{ and upper bound of heater voltage } V_{\rm H} \mbox{ vs. cold} \\ resistance \mbox{ RC}_{22}$ 



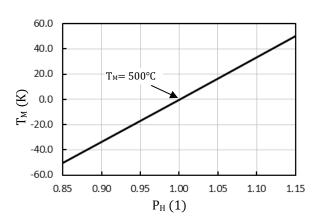


Relative change of membrane temperature ( $T_M$ ) by changing heater voltage ( $V_H$ )



 $\label{eq:mean1} Mean^1 \mbox{ and upper bound of heater power } P_H \mbox{ vs. cold} \\ resistance \mbox{ RC}_{22}$ 

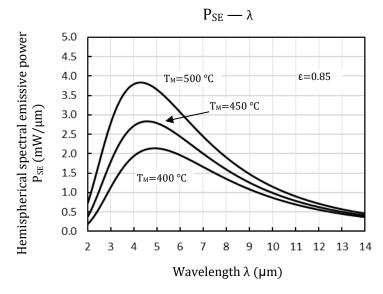




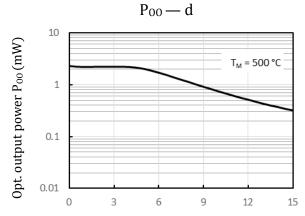
Relative change membrane temperature (T\_M) by changing heater power (P\_H)



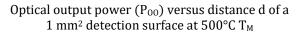
■ Typical Optical Characteristics (RO, T<sub>A</sub> = 22°C)

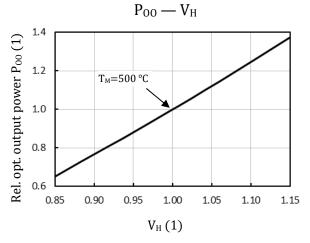


Hemispherical spectral emissive power of EMIRS200 chip surface with a typical emissivity (mean from 2 to 14  $\mu m$ ) of  $\epsilon{=}0.85$ 

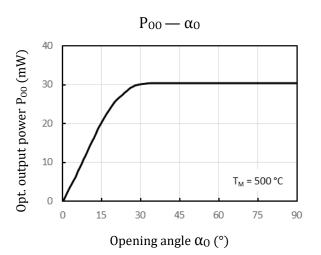


Distance d between EMIRS and detector (mm)

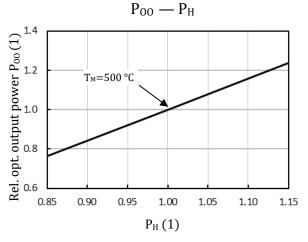




Relative change of optical output power ( $P_{00}$ ) by changing heater voltage ( $V_H$ )



Optical output power ( $P_{00})$  versus opening angle  $\alpha_0$  (integral rotation of a cone) at 500°C  $T_M$ 



Relative change of optical output power  $(P_{00})$  by changing heater power  $(P_H)$